

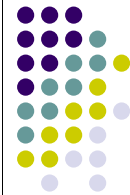
Chapter 6

z-Transform



Part C

The Transfer Function



Part C: The Transfer Function



- ◆ Definition
- ◆ Transfer Function Expression
- ◆ Frequency Response from Transfer Function
- ◆ Geometric Interpretation of Frequency Response Computation
- ◆ Stability Condition in Terms of Poles Locations

2. 1 Definition



- Z-transform $H(z)$ of the impulse response $h[n]$ of the filter is called the *transfer function* or the *system function*
- Generalization of the frequency response $H(e^{j\omega})$
- Derived through the method similar to that of the frequency response

2.1 Definition

- LTI discrete-time system

$$y[n] = \sum_{k=-\infty}^{\infty} h[k]x[n-k]$$

- Taking the DTFT

$$\begin{aligned} Y(e^{j\omega}) &= \sum_{n=-\infty}^{\infty} y[n]e^{-j\omega n} \\ &= \sum_{n=-\infty}^{\infty} \left(\sum_{k=-\infty}^{\infty} h[k]x[n-k] \right) e^{-j\omega n} \end{aligned}$$

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1. Definition

- Taking the z-Transform

$$\begin{aligned} Y(z) &= \sum_{n=-\infty}^{\infty} y[n]z^{-n} \\ &= \sum_{n=-\infty}^{\infty} \left(\sum_{k=-\infty}^{\infty} h[k]x[n-k] \right) z^{-n} \\ &= \sum_{k=-\infty}^{\infty} h[k] \left(\sum_{n=-\infty}^{\infty} x[n-k]z^{-n} \right) \\ &= \sum_{k=-\infty}^{\infty} h[k] \left(\sum_{l=-\infty}^{\infty} x[l]z^{-(l+k)} \right) \end{aligned}$$

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2.1 Definition

- Taking the z-Transform

$$\begin{aligned} Y(z) &= \sum_{k=-\infty}^{\infty} h[k] \left(\sum_{l=-\infty}^{\infty} x[l]z^{-l} \right) z^{-k} \\ &= \sum_{k=-\infty}^{\infty} h[k]z^{-k} X(z) \end{aligned}$$

$H(z)$

- Here $Y(z) = H(z)X(z)$

- Thus $H(z) = Y(z)/X(z) \xrightarrow{\text{IZT}} h[n]$

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2.2 Transfer function Expression

- **LTI FIR Digital Filter**

- **Impulse response**

$$h[n], \quad N_1 \leq n \leq N_2$$

- **Transfer function**

$$H(z) = \sum_{n=N_1}^{N_2} h[n]z^{-n}$$

- ※ All the poles of causal FIR digital filter are at $z=0$.

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2.1 Definition

Example :

- Consider the M -point **moving average** FIR filter with an impulse response

$$h(n) = \begin{cases} 1/M, & 0 \leq n \leq M-1 \\ 0, & \text{otherwise} \end{cases}$$

- Its transfer function is then given by

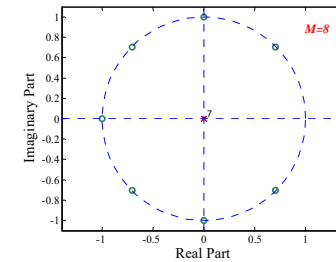
$$H(z) = \frac{1}{M} \sum_{n=0}^{M-1} z^{-n} = \frac{1-z^{-M}}{M(1-z^{-1})} = \frac{z^M - 1}{M \cdot z^{M-1}(z-1)}$$

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2.1 Definition

- The transfer function has M zeros on the unit circle at $z = e^{j2\pi k/M}$, $k = 0, \dots, M-1$
- There are poles at $z = 0$ and a single pole at $z = 1$

The pole at $z = 1$ exactly **cancels** the zero at $z = 1$. The ROC is the entire z -plane except $z = 0$



2.2 Transfer function Expression

• LTI IIR Digital Filter

- LTI discrete-time system characterized by a difference equation

$$\sum_{k=0}^N d_k y[n-k] = \sum_{k=0}^M p_k x[n-k]$$

- **Transfer function** : taking the z -transform and division

$$H(z) = \frac{\sum_{k=0}^M p_k z^{-k}}{\sum_{k=0}^N d_k z^{-k}}$$

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2.2 Transfer function Expression

• LTI IIR Digital Filter

- Or, equivalently as

$$H(z) = z^{(N-M)} \frac{\sum_{k=0}^M p_k z^{M-k}}{\sum_{k=0}^N d_k z^{N-k}}$$

- Alternate form

$$H(z) = \frac{p_0}{d_0} \frac{\prod_{k=0}^M (1 - \xi_k z^{-1})}{\prod_{k=0}^N (1 - \lambda_k z^{-1})} = z^{N-M} \frac{\prod_{k=0}^M (z - \xi_k)}{\prod_{k=0}^N (z - \lambda_k)}$$

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2.2 Transfer function Expression

Example :

- A **causal** LTI **IIR** digital filter is described by a constant coefficient difference equation, given by

$$y[n] = x[n-1] - 1.2x[n-2] + x[n-3] + 1.3y[n-1] - 1.04y[n-2] + 0.222y[n-3]$$
- Its transfer function is therefore given by

$$H(z) = \frac{Y(z)}{X(z)} = \frac{z^{-1} - 1.2z^{-2} + z^{-3}}{1 - 1.3z^{-1} + 1.04z^{-2} - 0.222z^{-3}}$$

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2.3 Frequency Response from Transfer Function

- If ROC of the transfer function $H(z)$ includes the **unit circle**, the frequency response $H(e^{j\omega})$ of the LTI digital filter can be obtained simply as follows:

$$H(e^{j\omega}) = H(z) \Big|_{z=e^{j\omega}}$$

- Transfer function $H(z)$ can be determined from its Fourier transform $H(e^{j\omega})$ by analytic continuation

$$H(z) = H(e^{j\omega}) \Big|_{\omega = \frac{1}{j} \ln z}$$

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2.2 Transfer function Expression

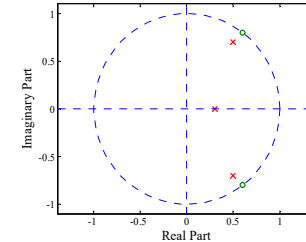
Example :

- Alternative form $H(z) = \frac{z^2 - 1.2z + 1}{z^3 - 1.3z^2 + 1.04z - 0.222}$

$$H(z) = \frac{(z - 0.6 + j0.8)(z - 0.6 - j0.8)}{(z - 0.3)(z - 0.5 + j0.7)(z - 0.5 - j0.7)}$$

- Zero-pole plot

□ ROC: $|z| > \sqrt{0.74}$



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2.3 Frequency Response from Transfer Function

- For a **stable** rational transfer function in the form

$$H(z) = \frac{p_0}{d_0} \cdot z^{(N-M)} \cdot \frac{\prod_{k=1}^M (z - \xi_k)}{\prod_{k=1}^N (z - \lambda_k)}$$

- The factored form of the frequency response is given by

$$H(e^{j\omega}) = \frac{p_0}{d_0} \cdot e^{j\omega(N-M)} \cdot \frac{\prod_{k=1}^M (e^{j\omega} - \xi_k)}{\prod_{k=1}^N (e^{j\omega} - \lambda_k)}$$

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2.3 Frequency Response from Transfer Function

- **zero factor** $(e^{j\omega} - \xi_k)$
- **pole factor** $(e^{j\omega} - \lambda_k)$
- The magnitude function is given by

$$\begin{aligned} |H(e^{j\omega})| &= \left| \frac{p_0}{d_0} \right| \left| e^{j\omega(N-M)} \right| \frac{\prod_{k=1}^M |e^{j\omega} - \xi_k|}{\prod_{k=1}^N |e^{j\omega} - \lambda_k|} \\ &= \left| \frac{p_0}{d_0} \right| \cdot \frac{\prod_{k=1}^M |e^{j\omega} - \xi_k|}{\prod_{k=1}^N |e^{j\omega} - \lambda_k|} \end{aligned}$$

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2.3 Frequency Response from Transfer Function

- The phase response for a rational transfer function is of the form

$$\begin{aligned} \arg H(e^{j\omega}) &= \arg(p_0 / d_0) + \omega(N - M) \\ &+ \sum_{k=1}^M \arg(e^{j\omega} - \xi_k) - \sum_{k=1}^N \arg(e^{j\omega} - \lambda_k) \end{aligned}$$

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2.3 Frequency Response from Transfer Function

- For a **real coefficient** transfer function, the magnitude-squared function

$$\begin{aligned} |H(e^{j\omega})|^2 &= \left| \frac{p_0}{d_0} \right|^2 \frac{\prod_{k=1}^M (e^{j\omega} - \xi_k)(e^{-j\omega} - \xi_k^*)}{\prod_{k=1}^N (e^{j\omega} - \lambda_k)(e^{-j\omega} - \lambda_k^*)} \\ &= H(e^{j\omega})H^*(e^{j\omega}) \\ &= H(e^{j\omega})H(e^{-j\omega}) = H(z)H(z^{-1}) \Big|_{z=e^{j\omega}} \end{aligned}$$

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2.3 Frequency Response from Transfer Function

- **Phase response** of an LTI discrete-time system with a **real-coefficient transfer function**

$$\theta(\omega) = \tan^{-1} \left[\frac{H_{\text{im}}(z)}{H_{\text{re}}(z)} \right]_{z=e^{j\omega}} = \frac{1}{2j} \ln \left[\frac{H(z)}{H(z^{-1})} \right]_{z=e^{j\omega}}$$

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2.3 Frequency Response from Transfer Function

- **Group delay** of an LTI discrete-time system with a **real-coefficient** transfer function

$$\tau_g(\omega) = -\frac{d\theta(\omega)}{d\omega} = -\operatorname{Re} \left(z \frac{d[\ln H(z)]}{dz} \right) \bigg|_{z=e^{j\omega}}$$

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2.4 Geometric Interpretation of Frequency Response Computation

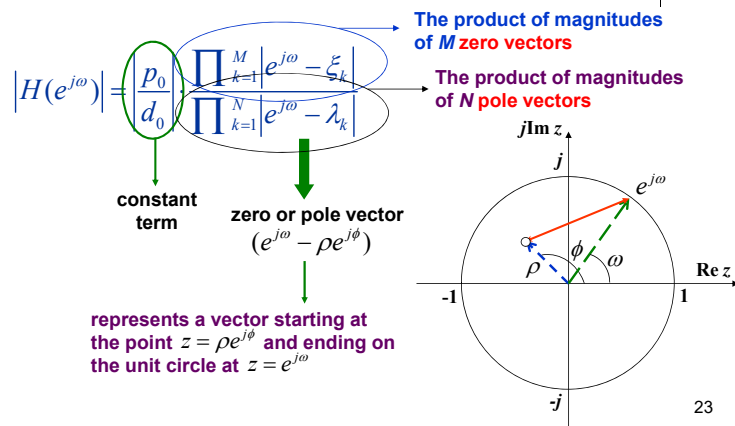
- For a **stable** rational transfer function in the form

$$H(e^{j\omega}) = \frac{p_0}{d_0} e^{j\omega(N-M)} \frac{\prod_{k=1}^M (e^{j\omega} - \xi_k)}{\prod_{k=1}^N (e^{j\omega} - \lambda_k)}$$

- Typical factor $e^{j\omega} - \rho e^{j\phi}$
 - Pole factor: $e^{j\omega} - \xi_k$
 - Zero factor: $e^{j\omega} - \lambda_k$

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2.4 Geometric Interpretation of Frequency Response Computation

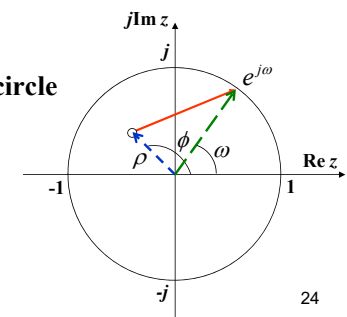


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2.4 Geometric Interpretation of Frequency Response Computation

- **As ω varies from 0 to 2π**

- Tip of the vector moves counterclockwise from the point $z = 1$ tracing the unit circle and back to the point $z = 1$.



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2.4 Geometric Interpretation of Frequency Response Computation



- Likewise, from

$$\arg H(e^{j\omega}) = \arg(p_0 / d_0) + \omega(N - M) + \sum_{k=1}^M \arg(e^{j\omega} - \xi_k) - \sum_{k=1}^N \arg(e^{j\omega} - \lambda_k)$$

- **Phase response** at a specific value of ω is obtained by
 - adding the phase of the term p_0 / d_0 and the linear-phase term $\omega(N - M)$ to the sum of the angles of the zero vectors minus the angles of the pole vectors.

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2.4 Geometric Interpretation of Frequency Response Computation



- Thus, an *approximate plot* of the **magnitude and phase responses** of the transfer function of an LTI digital filter can be developed by *examining the pole and zero locations*
- Now, a zero (pole) vector has the smallest (largest) magnitude when $\omega = \varphi$

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2.4 Geometric Interpretation of Frequency Response Computation



- To highly *attenuate* signal components in a specified frequency range, we need to **place zeros very close to or on the unit circle** in this range.
- Likewise, to highly *emphasize* signal components in a specified frequency range, we need to **place poles very close to the unit circle** in this range.

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2.5 Stability Condition in Terms of Poles Locations



- A **causal** LTI digital filter is **BIBO stable** if and only if its impulse response $h[n]$ is absolutely summable, i.e.,

$$S = \sum_{n=-\infty}^{\infty} |h(n)| < \infty$$

- We now develop a stability condition in terms of the pole locations of the transfer function $H(z)$

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2.5 Stability Condition in Terms of Poles Locations

- ROC of the z-transform $H(z)$
 - $|z|=r$ for which $h[n]r^n$ is absolutely summable
- Thus, if the ROC includes the unit circle $|z|=1$, then the digital filter is **stable**, and **vice versa**
- Meanwhile, for LTI system **causality** we require that $h[n]=0$, for $n < 0$. This implies that the ROC of $H(z)$ must be outside some circle of radius R_x .

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2.5 Stability Condition in Terms of Poles Locations

Theorem

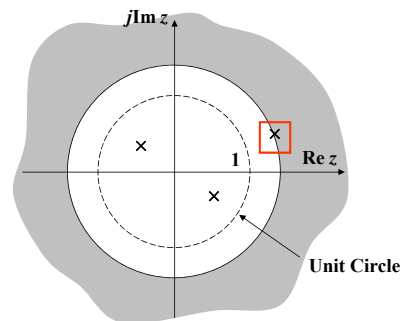
A causality LTI system is stable **if and only if** the system function $H(z)$ has **all its poles inside the unit circle**. So, the ROC will include the unit circle and entire z-plane including the point $z = \infty$

- *An causal FIR digital filter with bounded impulse response is always stable (?)*

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2.5 Stability Condition in Terms of Poles Locations

Proof: (Hint : reduction to absurdity)



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2.5 Stability Condition in Terms of Poles Locations

- On the other hand, an causal IIR filter may be unstable if not designed properly.
- Furthermore, an originally stable IIR filter characterized by **infinite precision coefficients** may become unstable when coefficients get **quantized** due to implementation

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2.5 Stability Condition in Terms of Poles Locations

Example 1:

Under what conditions, the following system is stable or causal ?

$$H(z) = \frac{-3z^{-1}}{2 - 5z^{-1} + 2z^{-2}}$$

Solution:

Step 1----Determine the zeros and poles of $H(z)$

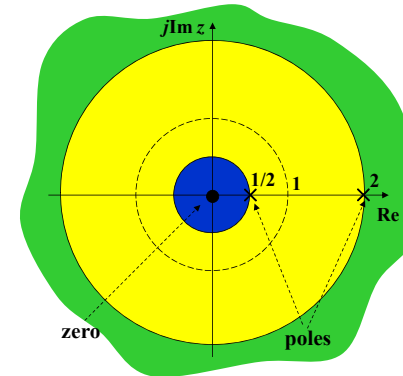
$$H(z) = \frac{-3z^{-1}}{2 - 5z^{-1} + 2z^{-2}} = \frac{-3z}{(2z-1)(z-2)}$$

$$z_{\text{zero}}=0, \quad z_{\text{pole}}=0.5, 2$$

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2.5 Stability Condition in Terms of Poles Locations

Step 2----plot the zeros and poles on the z-plane



Step 3----Determine all possible ROCs according to the distribution of the zeros and poles

ROC1={ $|z|<0.5$ }
—Blue Area

ROC2={ $0.5<|z|<2$ }
—yellow Area

ROC3={ $|z|>2$ }
—Green Area

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2.5 Stability Condition in Terms of Poles Locations

Step4----Discuss the system's stability and causality

Case 1: **ROC1**= $\{|z|<0.5\}$ Because the unit circle does not lie in this area and the ROC is inside of the circle with radius 0.5, the system is **anti-causal** and **unstable**.

Case 2: **ROC2**= $\{0.5<|z|<2\}$ Because the unit circle lies in this area and the ROC is an annulus bounded by 0.5 and 2, the system is **anti-causal** and **stable**.

Case 3: **ROC3**= $\{|z|>2\}$ Because the unit does not lie in this area and the ROC is outside of the circle with radius 2, the system is **causal** and **unstable**.

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2.5 Stability Condition in Terms of Poles Locations

Example 2:

Consider a causal LTI discrete-time system with an impulse response

$$h[n] = \alpha^n \mu[n]$$

• **Solution:** For this system

$$S = \sum_{n=-\infty}^{\infty} |\alpha^n \mu[n]| = \sum_{n=-\infty}^{\infty} |\alpha^n| = \frac{1}{1-|\alpha|}, \quad \text{if } |\alpha| < 1$$

- Therefore $S < \infty$ if $|\alpha| < 1$ for which the system is **BIBO stable**
- If $|\alpha| = 1$, the system is not BIBO stable.

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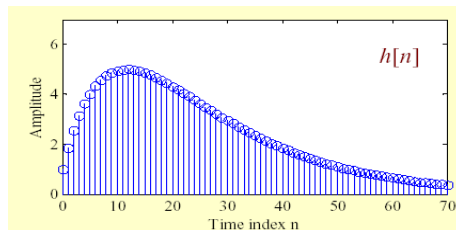
2.5 Stability Condition in Terms of Poles Locations

Example 3:

Consider a causal LTI discrete-time IIR system an

$$H(z) = \frac{1}{1 - 1.845z^{-1} + 0.850586z^{-2}}$$

The plot of impulse response is



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2.5 Stability Condition in Terms of Poles Locations

Example 3:

- The absolute summability condition is satisfied.

Hence, $H(z)$ is a stable transfer function.

- Now, consider the case when the transfer function coefficients are rounded to values with 2 digits after the decimal point:

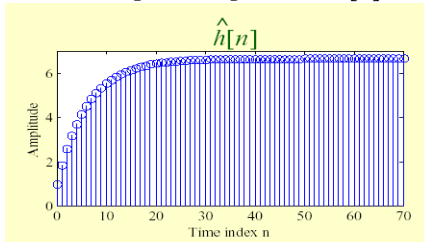
$$\hat{H}(z) = \frac{1}{1 - 1.85z^{-1} + 0.85z^{-2}}$$

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2.5 Stability Condition in Terms of Poles Locations

Example 3:

- The plot of the impulse response of $\hat{h}[n]$ is shown below



- Absolute summability condition is violated.

Thus, $\hat{H}(z)$ is an unstable transfer function

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2.5 Stability Condition in Terms of Poles Locations

Example 4:

Consider a causal LTI IIR discrete-time system with decaying impulse response

$$h[n] = \begin{cases} \frac{1}{n}, & n \geq 1 \\ 0, & n \leq 0 \end{cases}$$

- Solution $H(z) = \sum_{n=1}^{\infty} \frac{z^{-n}}{n} = \log_e \left(\frac{1}{1-z^{-1}} \right)$, which has infinite number of poles on the unit circle at $|z| = 1$ and hence, it is unstable.

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